The 3D Motorcycle Complex for Structured Volume Decomposition — Supplement —

A. Sparse Serial Motorcycle Complex

Let us expand on the remark in Sec. 4.2 about the alternative of a serial motorcycle complex construction. A proposal in [EGKT08, §7] for the 2D case is to trace motorcycles in a serial rather than simultaneous manner. While this voids canonicity[†], it enables the option to omit tracing motorcycles that would form removable (though not regular-removable) traces right away. For instance, if the two directions neighboring the next motorcycle's direction around a singularity have been traced (out of or into the singularity) already, the motorcycle can be omitted. The result (called *sparse MC* in the following) will be coarser, though not necessarily irreducible.

Following this idea, Alg. A is a modified variant of Alg. 1; the parametrization based Alg. 2 can be modified analogously. The key difference is that fire sources (facets incident at singularities) are processed one after the other, and those that are not necessary to establish a valid configuration around a singularity are skipped. In the loop (line 1) we prioritize edges that already have some incident burnt facets, and process facets f around an edge e in circular order.

The condition necessary(e, f) (line **2**) is defined as follows. Let $f_{-2}, f_{-1}, f, f_{+1}, f_{+2}$ denote the (possibly cyclically selfoverlapping) sequence of facets incident at singular edge *e* surrounding facet *f* (in either orientation). Condition necessary(e, f)is true iff either f_{-1} and f_{+1} are not burnt yet, or f_{-1} and f_{+2} are burnt but not f_{+1} , or f_{-2} and f_{+1} are burnt but not f_{-1} . In these cases *f* needs to be burnt (i.e., become part of the motorcycle complex as well) as well—otherwise the complex would contain cells

[†] While the simultaneously constructed 2D motorcycle graph yields a *canonical* decomposition, its serial construction voids this property due to order dependence. For 3D neither algorithm yields a canonical partition, as already the crucial 2D right hand arbitration rule does not extend to 3D.

Model	raw	МС	MCs	MC _{rs}	$\frac{MC}{MC_S}$	$\frac{MC}{MC}$
EXAMPLE 3	9087	2877	5125	2691	56.1%	106.9%
example 1	3137	1123	1199	962	93.7%	116.7%
EXAMPLE 2	233	87	280	101	31.1%	86.1%
DRAGON-HEX	979	357	399	317	89.5%	112.6
GARGOYLE	720	257	283	220	90.8%	116.8%
ANC101 A1	1359	460	524	422	87.8%	109.0%
FERTILITY-HEX	221	76	80	66	95.0%	115.2%
PEGASUS-HEX	1035	374	408	287	91.7%	130.3%
KISS HEX	543	200	244	189	82.0%	105.8%
ANC101	609	207	136	120	152.2%	172.5%
IMPELLER STRESSTEST	184	37	71	61	52.1%	60.7%
ARMADILLO HEX-A	680	266	292	227	91.1%	117.2%
ARMADILLO HEX-B	396	147	176	133	83.5%	110.5%
			:			
EXAMPLE 5	1	1	1	1	100.0	100.0%

Table A: Using the dataset from Table 1, reported are the number of blocks in the raw motorcycle complex (raw), fully reduced motorcycle complex (MC), sparse serial motorcycle complex (MCs) and its reduced version (MC_{rs})

with edges with inner angles of 270° (or larger) and would not be a pure cuboid block decomposition.

Algorithm A: Serial Motorcycle Complex of Hex Mesh					
1 foreach singular e and $f \in F_e$ do					
2 if necessary(e, f) then Q .push($(e, f, 0)$) // ignite					
while Q non-empty do					
$(e, f, d) \leftarrow Q.pop()$					
if alive(e) then // not crossing burnt terrain					
tag f // mark facet as burnt					
foreach regular interior edge $e' \neq e$ incident to					
f do					
if $opp(e', f)$ is not tagged then					
Q.push(e', opp(e', f), d+1) // spread					
foreach boundary facet f do tag f					

In essence, the algorithm attempts to omit "every other" (to the extent permitted by parity) wall around a singularity right away, rather than achieving this via reduction by wall retraction afterwards. Note that the incorporation of a similar omission strategy directly into the *non-serial* algorithm (as done for the 2D case in [SPGT18, §3.1]) would not be straightforward because the a priori omission decision cannot be made simply per singularity in isolation but would require some form of global coordination in the interconnected network of singular arcs in the 3D case.

The result is a block decomposition that can be expected to be coarser than the immediate result (without reduction by wall retraction) of the algorithms from Sec. 5. Indeed this is the case; however, our proposed *reduced* motorcycle complex typically is even simpler than this sparse serial motorcycle complex, as evident from Tables A and B. Of course reduction could also be applied to the sparse MC, but this yields no consistent benefit (last column).

Model	raw	МС	MCs	MC _{rs}	$\frac{MC}{MC_S}$	$\frac{MC}{MC_{rs}}$
ARMADILLO	392	132	207	121	63.8%	109.1%
BONE	57	15	25	18	60.0%	83.3%
BROKEN BULLET	25	5	11	9	45.5%	55.6%
CAMILLE HAND	75	26	42	27	61.9%	96.3%
CUBE SPHERE	10	4	6	6	66.7%	66.7%
CYLINDER	11	5	5	5	100.0%	100.0%
FANDISK	43	19	17	14	111.8%	135.7%
FANPART	5	3	5	3	60.0%	100.0%
JOINT	54	15	21	14	71.4%	107.1%
KITTEN	77	19	53	30	35.8%	63.3%
PRISMA	3	2	2	2	100.0%	100.0%
ROCKERARM	217	78	183	114	42.6%	68.4%
SCULPTURE	27	13	18	13	72.2%	100.0%
SPHERE	7	2	5	2	40.0%	100.0%
TETRAHEDRON	4	2	3	2	66.7%	100.0%

Table B: Using the dataset from Table 2, reported are the number of blocks in the raw motorcycle complex (raw), fully reduced motorcycle complex (MC), sparse serial motorcycle complex (MCs) and its reduced version (MC_{rs})

B. Constraint System Simplification

We show that, analogous to [MC19, §5.3], the 3D constraint system can be transformed such that only a small subsystem needs to be considered in the exact solver; all other variables are deduced in a back-substitution manner. The subsystem contains only the variables associated with node vertices. This shows that the small system set up in Sec. 6.2.2 is indeed sufficient.

At vertices not incident to any cut or align facets, incident tetrahedra form a single sector and hence, share parametrization values. The equations corresponding to edges incident to such vertices are trivially satisfied and can be left out of the system. This leaves us with a system over the variables of vertices on sheets.

Cut Sheets. For each sheet we can denote the parametrization variables of a vertex p in the two sectors on the two sides of the sheet as \boldsymbol{u}_p^+ and \boldsymbol{u}_p^- . Given a sheet with transition function π , the transition constraint for an edge *ab* on the sheet then has the form $\boldsymbol{u}_{b}^{+}-\boldsymbol{u}_{a}^{+}=\pi(\boldsymbol{u}_{b}^{-}-\boldsymbol{u}_{a}^{-}).$

Given a sequence of vertices $\boldsymbol{u}_0^{\pm}, \boldsymbol{u}_1^{\pm}, \dots, \boldsymbol{u}_n^{\pm}$ forming a chain of edges on a sheet, the equation corresponding to the *k*-th edge is: τ_k^w : $u_k^+ - u_{k-1}^+ = \pi(u_k^- - u_{k-1}^-).$

Cumulative sums of these equations have a simple form, namely

$$\sum_{i=1}^{k} \tau_{i}^{w} : \boldsymbol{u}_{k}^{+} - \boldsymbol{u}_{0}^{+} = \pi(\boldsymbol{u}_{k}^{-} - \boldsymbol{u}_{0}^{-}), \qquad (a)$$

All transition constraints of a sheet can hence be rewritten with respect to one selected base node vertex of the sheet, with variable u_0 . Re-ordering the variables in the system such that those corresponding to node sectors come last, the following structure is obtained per sheet: $u_0^- u_0^+$

$$\begin{bmatrix} 1 & -\pi & & & & & & \\ & \ddots & & \ddots & & & & \\ & 1 & -\pi & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ \end{array} \right)$$
(b)

where each entry is a 3×3 block (π : rotational matrix of transition; $\mathbf{l} = \text{diag}(1, 1, 1)$, because **u** has three components. The vertical bar separates non-node (left) from node vertex variables (right).

Align Sheets. Analogously, cumulative sums of alignment constraints can be built, forming this structure per align sheet:

$$\begin{bmatrix} \mathbf{1}^{k} & & & & & & & \\ & \ddots & & & & & & \\ & & & \mathbf{1}^{k} & & & -\mathbf{1}^{k} \\ & & & & & & & \\ & & & & & & \\ \end{array}$$
 (c)

where $\mathbf{1}^{k}$ is a 1 × 3 block: [1,0,0] for k = 0, [0,1,0] for k = 1, [0,0,1] for k = 2, where k is the aligned coordinate component.

Global System Combining these systems over all sheets will yield the global system. However, not all non-node vertex variables appear in only one of these systems. It is therefore not evident that the combined system maintains an upper triangular structure among the non-node vertices (the left parts in the above matrices). Concretely, among the non-node vertex variables, those on branches appear in two equations each, because each sector incident on an inner branch vertex is bounded by two sheets. We show that the union of these equations still forms an upper triangular system.

Given a cycle of n sheets incident on a branch with transition functions $\pi_1, \pi_2 \dots \pi_n$ and base node sector variables $\boldsymbol{u}_1^{\pm}, \boldsymbol{u}_2^{\pm} \dots \boldsymbol{u}_n^{\pm}$, respectively, the transition equation for a vertex with sector variables $\boldsymbol{p}_0, \boldsymbol{p}_1 \dots \boldsymbol{p}_{n-1}$ (see inset figure for n = 3) corresponding to the *k*-th sheet will be: $\boldsymbol{p}_k - \boldsymbol{u}_k^+ = \pi_k (\boldsymbol{p}_{k-1} - \boldsymbol{u}_k^-)$.



Via variable elimination and reordering these can be turned into an upper triangular structure, namely:

In case of a branch lying on the boundary, the sheets around it can be arranged such that the first and last are alignment sheets, i.e., $a_1, \boldsymbol{u}_1^{\pm}, \boldsymbol{u}_2^{\pm} \dots \boldsymbol{u}_{n-2}^{\pm}, a_2$. This yields a lower bidiagonal structure for the non-node variables (easily transformable into triangular form):

$$\begin{bmatrix} \mathbf{1}^{a_1} & & & & \mathbf{1}^{a_1} \\ -\pi_1 & \mathbf{1} & & & & \\ & \ddots & \ddots & & & \\ & & -\pi_{n-2} & \mathbf{1} & & \ddots & & \\ & & & & \mathbf{1}^{a_2} & & & \mathbf{1}^{a_2} \end{bmatrix}$$
(e)

Globally ordering all variables in the system such that those corresponding to node sectors come last, the cumulative transition and alignment equations form the following constraint system:



where all the sub matrices A_i are upper triangular (formed by the left parts of the above matrices), containing constraints corresponding to, respectively, non-branch sheet vertices (b)+(c), non-node interior branch vertices (d), and non-node boundary branch vertices (e). The small block C is exactly the system we set up and solve in Sec. 6.2.2, and the described simple subsequent propagation process corresponds to back-substitution through B and A_i to the nonnode vertex variables.

C. Complete Version of Table 1

Model	BC	BC^{-}	raw	MC ⁺	MC ⁺	Т	MC	MC BC
2018 - Fuzzy clustering based pseudo-swept volume decomposition for hexahedral meshing_Example_3	406136	67828	9087	5780	1.42%	41.63%	2877	0.71%
2018 - Fuzzy clustering based pseudo-swept volume decomposition for hexahedral meshing_Example_1	74331	11385	3137	2248	3.02%	15.09%	1123	1.51%
2018 - FUZZY CLUSTERING BASED PSEUDO-SWEPT VOLUME DECOMPOSITION FOR HEXAHEDRAL MESHING_EXAMPLE_2	3253	678	233	195	5.99%	13.67%	87	2.67%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_DRAGON-HEX 2014 - 11 - BASED CONSTRUCTION OF POLYCUBE MARS ERON COMPLEY SUARES, GARGOVLE	12488	2959	979 720	724 546	5.8%	30.33%	357	2.86%
2011 - ALL-HEX MESH GENERATION VIA VOLUMETRIC POLYCUBE DEFORMATION_ANC101_A1	12336	3118	1359	846	6.86%	45.33%	460	3.73%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_FERTILITY-HEX	2002	548	221	189	9.44%	27.02%	76	3.8%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_PEGASUS-HEX	9745	2415	1035	729	7.48%	36.29%	374	3.84%
2016 - EFFCIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_KISS_HEX 2014 - LI BASED CONSTRUCTION OF POLYCUBE MAPS EFFORM COMPLEY SHARES, ANC 101	5019	1194	543	385	6.03%	39.3%	200	3.98%
2015 - PRACTICAL HEX-MESH OPTIMIZED WARD REGENERATION CONFIGURATION IMPELIER STRESSTEST IN	878	1285	184	124	14.12%	23,86%	37	4.21%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_IMPELLER_STRESSTEST_OUT	878	176	184	124	14.12%	23.86%	37	4.21%
2012 - ALL-HEX MESHING USING SINGULARITY-RESTRICTED FIELD_IMPELLER	878	182	184	124	14.12%	23.86%	39	4.44%
2016 - EFFCIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_ARMADILLO_HEX-A	5960	1491	680	516	8.66%	34.19%	266	4.46%
2010 - LI-LBASED CONSTRUCTION OF POLYCUBE MAP CONSTRUCTION_ARMADILLO_HEA-B 2014 - LI-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES DANCING-CHILDREN-2	5482	1516	672	533	9.07%	32.9%	259	4.72%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_DANCINGCHILDREN_IN	5482	1406	703	546	9.96%	34.52%	274	5%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_DANCINGCHILDREN_OUT	5482	1406	703	546	9.96%	34.52%	274	5%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_CHINESE-LION-HEX	6235	1468	818	589	9.45%	38.82%	321	5.15%
2016 - EFFCIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_DANCING_CHILDREN_HEX 2012 - ALL-HEY MESUNG USING SINGUL APITY-PERSTRUCTED FEELD FEETUL TY	4/55	342	682 234	532	13.01%	31.97%	247	5.19%
2015 - PRACTICAL HEX-MESHING OSING OF MICE AND THE STRUCTED FIELD FIELD FEELD FRAME	2112	348	308	265	12.55%	24.53%	114	5.4%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_ARMADILLO_OUT	2112	348	308	265	12.55%	24.53%	114	5.4%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_ARMADILLO_STRESSTEST_IN	2112	348	308	265	12.55%	24.53%	114	5.4%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_ARMADILLO_STRESSTEST_OUT	2112	348	308	265	12.55%	24.53%	114	5.4%
2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES_COGNIT 2016 - FERCIENT VOLUMETER: POLYCUBE-MAP CONSTRUCTION DEAGON HEX	3655	853	759 569	574 442	12.09%	32.35% 28.81%	298	5.74%
2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES ELEPHANT	2842	692	415	346	12.17%	28.97%	167	5.88%
2016 - Efficient Volumetric PolyCube-Map Construction_Elephant_hex	3105	770	527	399	12.85%	29.15%	189	6.09%
2016 - EFFICIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_BUNNY_HEX	1282	348	257	187	14.59%	30.74%	80	6.24%
2011 - ALL-HEX MESH GENERATION VIA VOLUMETRIC POLYCUBE DEFORMATION, KISS_HEX_COARSE	3690	1023	557	402	10.89%	38.44%	231	6.26%
2015 - FRACTICAL HEX-MIESH OPTIMIZATION VIA EDGE-CONE RECIFICATION_DRAGON_IN 2015 - PRACTICAL HEX-MISSI OPTIMIZATION VIA EDGE-CONE RECIFICATION DRAGON OUT	2019	495	340	220	10.9%	27.43%	127	6.29%
2011 - All-Hex Mesh Generation via Volumetric PolyCube Deformation_casting	2805	701	524	409	14.58%	29.47%	185	6.6%
2011 - All-Hex Mesh Generation via Volumetric PolyCube Deformation_kiss_hex	3690	1075	688	434	11.76%	39.25%	255	6.91%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_CHINESE_DRAGON_POLYCUBE_IN	810	189	174	147	18.15%	22.66%	56	6.91%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_GRAVLOC-HEX 2013. POLYCUT, MONOTONE GAADH, CUTE FOR POLYCUBE BASE COMPLEX CONSTRUCTION, CAPTER, HEX, OPT	3183	635	604 537	4/7	14.99%	27.97%	222	6.97%
2013 - I LL-HEX MESH GENERATION VIA VOLUMETRIC POLYCUBE DEFORMATION STAB3 REFINE3	2300	580	419	290	13.02%	36.08%	162	7.32%
2011 - All-Hex Mesh Generation via Volumetric PolyCube Deformation_bunny_hex	1324	373	275	194	14.65%	31.87%	97	7.33%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_ROCKERARM_MODEL_IN	678	152	162	130	19.17%	25.86%	50	7.37%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SUFFACES AND VOLUMES_ROCKERARM_POLYCUBE_IN	678	152	162	130	19.17%	25.86%	50	7.37%
2017 - A GUDAL APPROACH TO MULTI-AAIS SWEET MASS GENERATION_EAAMPLE_4 2014 - L1-BASED CONSTRUCTION OF POLYCIBE MASS FROM COMPLEX SHAPES DRAGON	3977	998	836	661	16.62%	24.19%	301	7.57%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_ROCKERARM-HEX	1202	306	223	181	15.06%	28.03%	91	7.57%
2017 - A GLOBAL APPROACH TO MULTI-AXIS SWEPT MESH GENERATION_EXAMPLE_1	1037	243	225	150	14.46%	22.32%	81	7.81%
2016 - EFFICIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_BUSTE_HEX	1081	275	244	182	16.84%	32.4%	85	7.86%
2016 - EHTCLENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_GREEK_SCULPTURE_HEX 2010 - SINGULAPITY STDUCTIDE SIMPLIFICATION OF HEYAHEDPAIL MESH VIA WEIGUHED PANKING, DECKEL INPUT 2010 - SINGULAPITY STDUCTIDE SIMPLIFICATION OF HEYAHEDPAIL MESH VIA WEIGUHED PANKING, DECKEL INPUT 2010 - SINGULAPITY STDUCTIDE SIMPLIFICATION OF HEYAHEDPAIL MESH 2010 - SINGULAPITY STDUCTIDE SIMPLIFICATION OF HEYAHEDPAIL MESH 2010 - SINGULAPITY STDUCTIDE SIMPLIFICATION OF HEYAHEDPAIL MESH 2010 - SINGULAPITY STDUCTION SINGULAPITY 2010 - SINGULAPITY SITUCTION SINGULAPITY 2010 - SIN	53116	12557	10922	8823	16.53%	28.44%	4249	7.99%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES BUNNY MODEL IN	637	141	151	124	19.47%	26.89%	51	8.01%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_BUNNY_POLYCUBE_IN	637	141	151	124	19.47%	26.89%	51	8.01%
2016 - EFFICIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_CARTER_HEX	2788	616	630	450	16.14%	34.55%	228	8.18%
2013 - POLYCUT - MONOTONE GRAPH-CUTS FOR POLYCUBE BASE-COMPLEX CONSTRUCTION_BU_HEX_OPT 2014 - 11-BASED CONSTRUCTION OF POLYCUBE MASE FROM COMPLEY SUARES POCKEDAEM 2	580	141	132	113	19.48%	27.21%	48	8.28%
2016 - Efficient Volumeric PolycereMap Construction Binda Hex-c	760	176	204	146	19.21%	30.68%	68	8.95%
2012 - ALL-HEX MESHING USING SINGULARITY-RESTRICTED FIELD_ROCKERARM	578	135	150	120	20.76%	30.66%	52	9%
2011 - ALL-HEX MESH GENERATION VIA VOLUMETRIC POLYCUBE DEFORMATION_BUMPY_TORUS	2518	631	595	446	17.71%	32.19%	228	9.05%
2011 - ALL-HEX MESH GENERATION VIA VOLUMETRIC POLYCUBE DEFORMATION, BU_REMESH_HEX	1098	308	301	202	18.4%	33.15%	102	9.29%
2017 - A GLOBAL APPROACH 10 MULTI-AXIS SWEPT MESH GENERATION_EXAMPLE_5	801	280	222	264	25.55%	32 19%	75	9.36%
2016 - Efficient Volumetric PolyCube-Map Construction_Rocker_Hex	730	187	199	156	21.37%	28.02%	69	9.45%
2017 - A GLOBAL APPROACH TO MULTI-AXIS SWEPT MESH GENERATION_EXAMPLE_2	974	224	288	202	20.74%	24.89%	95	9.75%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_TEAPOT_MODEL_IN	328	68	108	89	27.13%	28.6%	32	9.76%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_TEAPOT_POLYCUBE_IN 2014 - 11 BASED CONSTRUCTION OF POLYCUBE MARS ERON COMPLEY SURFACES AND VOLUMES_TEAPOT_POLYCUBE MARS	328	68	108	489	21.13%	28.6%	32	9.76%
2013 - POLYCUT - MONOTONE GRAPH-CUTS FOR POLYCUBE BASE-COMPLEX STATES DUM I _ TOKOS	664	176	184	138	20.78%	28.81%	67	10.09%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_KITTEN-HEX	208	57	71	57	27.4%	24.66%	21	10.1%
2016 - Skeleton-driven Adaptive Hexahedral Meshing of Tubular Shapes_warrior_graded	4869	1306	1447	1282	26.33%	30.81%	492	10.1%
2019 - DUAL SHEET MESHING - AN INTERACTIVE APPROACH TO ROBUST HEXAHEDRALIZATION_FANDISK.LIU18 2014 - LI PAGED CONSTRUCTION OF DOUCLUE MARS FROM COMPLEX SHARES AND L. 1	1284	20	35	26	29.21%	13.66%	121	10.11%
2014 - LI-BASED CONSTRUCTION OF POLYCOBE MAPS FROM COMPLEX SHAPES_ANGEL_1 2016 - ATTACATED_LEY 2016 - ATTACATED_LE	1284	235	362	266	20.72%	34.99%	131	10.2%
2016 - SKELETON-DRIVEN ADAPTIVE HEXAHEDRAL MESHING OF TUBULAR SHAPES_DINOPET_GRADED	2253	617	721	630	27.96%	32.67%	234	10.39%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_BUST_IN	494	102	128	110	22.27%	27.34%	52	10.53%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_BUST_OUT	494	102	128	110	22.27%	27.34%	52	10.53%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_KINGKONG_IN 2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_KINGKONG_OUT	180	45	71	62	34.44% 34.44%	25%	19	10.56%
2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES KISS	1896	567	560	418	22.05%	32.88%	205	10.30%
2016 - Skeleton-driven Adaptive Hexahedral Meshing of Tubular Shapes_dino_graded	904	275	306	261	28.87%	33.99%	99	10.95%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_FERTILITY_1	301	73	119	105	34.88%	22.71%	33	10.96%
2019 - SELECTIVE PADDING FOR POLYCUBE-BASED HEXAHEDRAL MESHING_DOUBLE_HINGE_WH	153	16	43	43	28.1%	10%	17	11.11%
2010 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_FERTILITY_2 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_FERTILITY_3	301	50	119	105	34.88%	22.71%	34	11.3%
2013 - POLYCUT - MONOTONE GRAPH-CUTS FOR POLYCUBE BASE-COMPLEX CONSTRUCTION_BUNNY_HEX_OPT	580	120	170	127	21.9%	30.17%	66	11.38%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_ASM_MODEL_OUT	122	33	68	64	52.46%	14.29%	14	11.48%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_ASM_POLYCUBE_OUT	122	33	68	64	52.46%	14.29%	14	11.48%
2017 - HEXAHEDRAL MESH GENERATION VIA CONSTRAINED QUADRILATERALIZATION_JOINT 2016 - POLYCURE SIMPLIFICATION FOR COARSE LAYOUTS OF SUPPACES AND VOLUMES, FANDISK, DOLYCUPE, IN	229	18	41	27	32.53% 30.57%	15.43%	10	12.05%
2010 TOPICODE SIMI ENTERTOR FOR COARSE EATOUTS OF SURFACES AND YOLUMES_FANDISK_FOLICOBE_IN	229	49	09	10	50.5170	21.40/0	29	12.00 /0

Table C: Statistics on a dataset of hexahedral meshes. Numbers of blocks in the base complex (BC), reduced base complex (BC^-), raw motorcycle complex (raw), reduced motorcycle complex with preserved singularity-adjacent walls (MC^+), fully reduced motorcycle complex (MC), percentage of arcs that are T-arcs (T).

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Madel	BC	BC-	P011/	MC ⁺	MC*	т	MC	мс
2014 - 1 1-RASED CONSTRUCTION OF POLYCURE MARS FROM COMPLEY SUARES, ROCKER ARM, 1	686	183	247	186	BC 27.11%	27.02%	87	BC 12.68%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_CAP_IN	327	97	124	92	28.13%	34.55%	42	12.84%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_CAP_OUT	327	97	124	92	28.13%	34.55%	42	12.84%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_ROCKERARM_MODEL_OUT	316 693	153	243	202	36.71%	16.14%	41	12.97%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_ROCKERARM_POLYCUBE_OUT	348	60	132	117	33.62%	19.5%	46	13.22%
2016 - EFFICIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_BIMBA_HEX-D	196	60	97	63	32.14%	23.77%	26	13.27%
2019 - SELECTIVE PADDING FOR POLYCUBE-BASED HEXAHEDRAL MESHING_LEGO_L2	525	83	221	167	31.81%	29.6%	70	13.33%
2019 - DORE SHEET MESHING - AN INTERACTIVE APPROACH TO ROBOST HEAAHEDRALIZATION_PANDISK 2016 - EFFICIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION BLADE HEX	389	90	142	130	33.42%	20.78%	53	13.62%
2016 - EFFICIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_FERTILITY_HEX-LARGEL	633	148	244	211	33.33%	22.91%	87	13.74%
2016 - EFFICIENT VOLUMETRIC POLYCUBE-MAP CONSTRUCTION_FERTILITY_HEX-SMALL	621	158	243	210	33.82%	23.37%	87	14.01%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF MEXAHEDRAL MESH VIA WEIGHTED KANKING_FERTILITY_INPUT 2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES ANGEL 2	302	75	116	103	34.09%	23.08%	43	14.10%
2019 - SELECTIVE PADDING FOR POLYCUBE-BASED HEXAHEDRAL MESHING_DOUBLE_HINGE_NH	105	15	35	35	33.33%	6.67%	15	14.29%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_TABLE1_POLYCUBE_IN	195	42	93	80	41.03%	25.17%	28	14.36%
2011 - ALL-HEX MESH GENERATION VIA VOLUMETRIC POLYCUBE DEFORMATION_FERTILITY_REFINE 2014 - 1 1-Based Construction of Polycure Maps from Complex Shapes, canewy	598 879	243	24.3	209	34.95%	24.86%	128	14.55%
2019 - DUAL SHEET MESHING - AN INTERACTIVE APPROACH TO ROBUST HEXAHEDRALIZATION_HANGER	41	11	30	20	48.78%	15.33%	6	14.63%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED RANKING_BUSTE_INPUT	18355	4925	7667	6570	35.79%	30.83%	2722	14.83%
2012 - ALL-HEX MESHING USING SINGULARITY-RESTRICTED FIELD_BUNNY 2010 - Selective Padding for Polycupe Rased Hexahedral Meshing Joint	259	52	101	93	35.91%	19.65%	39	15.06%
2019 - SELECTIVE FADDING FOR FOLFCOBE-DASED HEXAREDIKAL MESHING_JOINT	66	9	37	27	40.91%	18.09%	10	15.15%
2019 - DUAL SHEET MESHING - AN INTERACTIVE APPROACH TO ROBUST HEXAHEDRALIZATION_JOINT	59	10	33	24	40.68%	10.37%	9	15.25%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_HOLLOW-EIGHT-HEX	249	61	108	76	30.52%	39.2%	38	15.26%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED RANKING_BUSTE_OUTPUT	190	45	90	82	43.16%	17.75%	29	15.26%
2010 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_CAT_2_FABLED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2017 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2017 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2017 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2017 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2017 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2017 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2017 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2017 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING DOLPHIN PADDED 2017 - STRUCTURED VOLUME DECOMPOSITION VOLUME DECOMPOSITION VOLUME DECOMP	19	3	19	14	73.68%	23.29%	3	15.79%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_FEMUR1_PADDED	19	3	19	14	73.68%	23.29%	3	15.79%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_RABBIT_PADDED	19	3	19	14	73.68%	23.29%	3	15.79%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_ROTELLIPSE_PADDED 2016 - POLYCURE SIMPLIERCATION FOR COARSE LAVOUTS OF SURFACES AND VOLUMES ASM. MODEL IN	19	3	19	14	73.68%	23.29%	3	15.79%
2010 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_ASM_MODEL_IN 2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_ASM_MODEL_IN	200	52	80	66	33%	23.08%	32	16%
2019 - SELECTIVE PADDING FOR POLYCUBE-BASED HEXAHEDRAL MESHING_BEARING	184	46	70	64	34.78%	12.73%	30	16.3%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_FEMUR_MODEL_OUT	110	29	57	55	50%	16.48%	18	16.36%
2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES_FERTILITY	460	124	212	188	40.87%	20.33%	76	16.52%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED KANKING_PIG_001P01 2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCURE JOINT-HEX	59	10	420	22	37.29%	15.72%	140	16.95%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_CUBESPIKES_MODEL_IN	276	53	123	105	38.04%	21.02%	47	17.03%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_CUBESPIKES_POLYCUBE_IN	276	53	123	105	38.04%	21.02%	47	17.03%
2012 - ALL-HEX MESHING USING SINGULARITY-RESTRICTED FIELD_ELLIPSOID-A	34	7	27	14	41.18%	32.18%	6	17.65%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED KANKING_BOTTLE2_OUTPUT 2012 - ALL-HEX MESHING USING SINGULARITY-RESTRICTED FIELD HANGER	50	7	27	22	49.37%	16.08%	9	17.92%
2012 - ALL-HEX MESHING USING SINGULARITY RESTRICTED FIELD_JOINT	83	21	47	28	33.73%	17.8%	15	18.07%
2017 - HEXAHEDRAL MESH GENERATION VIA CONSTRAINED QUADRILATERALIZATION_PONE.0177603.s003	83	21	47	28	33.73%	17.8%	15	18.07%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED RANKING_TOY2_INPUT	14288	3857	7161	6153	43.06%	30.76%	2585	18.09%
2010 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_TABLET_POLYCUBE_OUT	149	46	79	67	40.32%	18.01%	27	18.12%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED RANKING_TOY1_INPUT	18883	5246	9461	8122	43.01%	29.98%	3427	18.15%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_FEMUR_POLYCUBE_OUT	110	30	57	55	50%	16.48%	20	18.18%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_BUNNY_MODEL_OUT	197	53	109	99	50.25%	13.94%	36	18.27%
2010 - I DEPEORE SIMPLIFICATION FOR COARSE LATOUTS OF SURFACES AND VOLUMES_BONNT_FOLTCODE_OUT 2012 - ALL-HEX MESHING USING SINGULARITY-RESTRICTED FIELD FANDISK	49	11	25	22	44.9%	11.61%	9	18.37%
2017 - HEXAHEDRAL MESH GENERATION VIA CONSTRAINED QUADRILATERALIZATION_FANDISK	49	11	28	22	44.9%	11.61%	9	18.37%
2017 - HEXAHEDRAL MESH GENERATION VIA CONSTRAINED QUADRILATERALIZATION_PONE.0177603.s002	49	16	27	22	44.9%	11.61%	9	18.37%
2019 - DUAL SHEET MESHING - AN INTERACTIVE APPROACH TO KOBUST HEXAHEDRALIZATION_ROCKARM 2016 - POLYCURE SIMPLIFICATION FOR COARSE LAYOUTS OF SUPEACES AND VOLUMES, HAND, MODEL, IN	172	35	59 81	41	34.45% 44.77%	18.12%	32	18.49%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES HAND POLYCUBE IN	172	35	81	77	44.77%	17.77%	32	18.6%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED RANKING_PIG_INPUT	13987	3768	7144	6078	43.45%	30.98%	2610	18.66%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED RANKING_BOTTLE2_INPUT	35860	9968	19360	16349	45.59%	31.63%	6816	19.01%
2010 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_KITTEN_WITH_BIFUR_2 2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED RANKING DECKEL OUTPUT	20	237	450	382	84.62% 47.39%	24.24%	155	19.23%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_FEMUR_MODEL_IN	145	36	63	59	40.69%	21.74%	28	19.31%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_FEMUR_POLYCUBE_IN	145	36	63	59	40.69%	21.74%	28	19.31%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_ROCKERARM_3	82	16	57	53	64.63%	22.83%	16	19.51%
2012 - ALL-HEX MESHING USING SINGULARITY-RESTRICTED FIELD_SCULPTORE-A 2011 - ALL-HEX MESH GENERATION VIA VOLUMETRIC POLYCUBE DEFORMATION ASM001	122	28	68	64	52.46%	14.29%	24	19.67%
2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES_ROD	122	30	70	64	52.46%	14.29%	24	19.67%
2017 - EXPLICIT CYLINDRICAL MAPS FOR GENERAL TUBULAR SHAPES_CACTUS	81	21	57	51	62.96%	21.54%	16	19.75%
2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES_BUSTE 2015 PRACTICAL HEY MESH OPTIMIZATION VIA EDGE CONE RECTIFICATION HANGER STRESSTERT IN	361	99	203	166	45.98%	21.07%	72	19.94%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_HANGER_STRESSTEST_IN	50	10	28	21	42%	15.94%	10	20%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_CHINESE_DRAGON_POLYCUBE_OUT	295	70	151	132	44.75%	18.73%	59	20%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_TEAPOT_MODEL_OUT	193	43	98	88	45.6%	21.76%	39	20.21%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_TEAPOT_POLYCUBE_OUT 2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_REOCK_MODEL_IN	193	43	98	88	45.6%	21.76%	39	20.21%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_BLOCK_MODEL_IN	162	42	109	105	64.81%	8.66%	33	20.37%
2019 - SELECTIVE PADDING FOR POLYCUBE-BASED HEXAHEDRAL MESHING_LEGO_L0	983	236	627	604	61.44%	13.82%	205	20.85%
2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED RANKING_EIGHT_INPUT	3867	1076	2250	1963	50.76%	24.04%	813	21.02%
2010 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_TWISTEDU 2016 - Skeleton-driven Adaptive Hexahedral Meshing of Turul ar Shapes_armadil 1.0	301	4	19	14	73.68% 54.82%	25.29% 7.49%	4 64	21.05%
2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES_BUNNY	273	73	157	129	47.25%	21.89%	59	21.61%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_BUNNY_IN	273	74	153	128	46.89%	20.42%	59	21.61%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_BUNNY_OUT	273	74	153	128	46.89%	20.42%	59	21.61%
2012 - ALL-DEA MESHING USING SINGULARITY-KESTRICTED FIELD_BONE 2019 - SINGULARITY STRUCTURE SIMPLIFICATION OF HEXAHEDRAL MESH VIA WEIGHTED RANKING FERTILITY OUTPUT	87	15	222	43	49.43%	6,93%	68	21.84%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES TABLE2 POLYCUBE IN	90	26	61	56	62.22%	11.51%	20	22.22%

Table C: Statistics on a dataset of hexahedral meshes. Numbers of blocks in the base complex (BC), reduced base complex (BC^-), raw motorcycle complex (raw), reduced motorcycle complex with preserved singularity-adjacent walls (MC^+), fully reduced motorcycle complex (MC), percentage of arcs that are T-arcs (T).

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Model	BC	BC ⁻	raw	MC+	MC* BC	Т	мс	MC BC
2019 - Selective Padding for Polycube-Based Hexahedral Meshing_Chamfer_L4	22	5	11	11	50%	6.02%	5	22.73%
2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES_KITTY	121	28	68	59	48.76%	23.13%	28	23.14%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_ROCKERARM_2 2019SINGULARITY STRUCTURE SIMPLIEGATION OF HEVANEDRAL MEGUTIA WEIGHTED RANKING, EIGHT, OUTPUT 2019SINGULARITY STRUCTURE SIMPLIEGATION OF HEVANEDRAL	82 43	17	35	35	64.63% 81.4%	22.83%	19	23.17%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING KITTEN_WITH_BIFUR_PADDED	82	16	57	53	64.63%	22.83%	20	24.39%
2016 - Structured Volume Decomposition via Generalized Sweeping_rockerarm_1	82	18	57	53	64.63%	22.83%	20	24.39%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_HAND7_PADDED	159	36	102	91	57.23%	23.29%	39	24.53%
2019 - SELECTIVE PADDING FOR POLYCUBE-BASED HEXAHEDRAL MESHING_WRENCH 2012 - ALL URE MESHING USING SINGU ADITY DESERTION OF DELID SCHLDRIDE R	61	13	32	30	49.18%	6.48%	15	24.59%
2019 - SILGULARING USING USI	144	35	113	104	72.22%	11.09%	36	24.04%
2019 - Dual Sheet Meshing - An Interactive Approach to Robust Hexahedralization_bunny	34	7	20	17	50%	8.89%	9	26.47%
2016 - Skeleton-driven Adaptive Hexahedral Meshing of Tubular Shapes_dinopet	117	31	113	109	93.16%	5.98%	31	26.5%
2016 - SKELETON-DRIVEN ADAPTIVE HEXAHEDRAL MESHING OF TUBULAR SHAPES_BIG_BUDDY	124	36	101	88	70.97%	10.89%	33	26.61%
2010 - Skeleton-Driven Adaptive Hexahedral Meshing of Tubular Shapes_Rocker_arm 2019 - Sfective Padding for Polycine-Rasped Hexahedral Meshing Chamfer I.0	29	13	18	18	62 07%	2 48%	12	20.07%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_KNOT-HEX	50	16	40	40	80%	15.79%	14	28%
2014 - L1-BASED CONSTRUCTION OF POLYCUBE MAPS FROM COMPLEX SHAPES_ANGEL_3	78	22	64	54	69.23%	17.8%	22	28.21%
2012 - ALL-HEX MESHING USING SINGULARITY-RESTRICTED FIELD_ELLIPSOID-B	7	2	7	7	100%	0%	2	28.57%
2012 - ALL-HEX MESHING USING SINGULARITY-KESTRICTED FIELD_ELLIPSOID-C 2016 - Skelfford John A DAPTive Hey Anterpart Mesunic of Them a Subject warding	287	2	262	254	100%	0% 5.99%	82	28.57%
2016 - Skeletion-Driven Adaptive Incareducal Meshing of Tubular Shapes Blood Vessel	52	17	48	48	92.31%	5.77%	15	28.85%
2017 - HEXAHEDRAL MESH GENERATION VIA CONSTRAINED QUADRILATERALIZATION_CUBE	17	5	16	13	76.47%	8.7%	5	29.41%
2017 - HEXAHEDRAL MESH GENERATION VIA CONSTRAINED QUADRILATERALIZATION_PONE.0177603.s001	17	5	14	13	76.47%	8.7%	5	29.41%
2012 - ALL-HEX MESHING USING SINGULARITY-RESTRICTED FIELD_DOUBLE	71	19	52	41	57.75%	25.25%	21	29.58%
2016 - SKELETON-DRIVEN ADAPTIVE HEXAHEDRAL MESHING OF TUBULAR SHAPES_CACTUS 2016 - SKELETON DRIVEN ADAPTIVE HEXAHEDRAL MESHING OF TUBULAR SHAPES_CIFE	37	11	3.5	33	89.19%	8.11%	11	29.73%
2016 - Skeleton-Driven Adartive Hexanedral Meshing of Tubular Shares_CLEP	47	14	47	47	100%	0%	14	29.79%
2016 - Skeleton-driven Adaptive Hexahedral Meshing of Tubular Shapes_octopus	104	30	75	69	66.35%	9.68%	31	29.81%
2016 - Structured Volume Decomposition via Generalized Sweeping_hand7_3	67	20	46	40	59.7%	16.38%	20	29.85%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_HAND_MODEL_OUT	107	32	74	70	65.42%	14.33%	32	29.91%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_HAND_POLYCUBE_OUT 2017 EXPLORE OF UNDERGAL MADE FOR CONDEND TO THE SURFACES AND VOLUMES_HAND_POLYCUBE_OUT	107	32	24	22	65.42%	14.33%	32	29.91%
2017 - EXPLICIT CTLINDRICAL MAPS FOR GENERAL TOBULAR SHAPES FEMUR SHELL 2017 - EXPLICIT CYLINDRICAL MAPS FOR GENERAL TUBULAR SHAPES FEMUR SHELL 2	30	8	24	22	73.33%	11.76%	9	30%
2019 - Singularity Structure Simplification of Hexahedral Mesh via Weighted Ranking_toy2_output	129	34	94	88	68.22%	12.47%	39	30.23%
2019 - SELECTIVE PADDING FOR POLYCUBE-BASED HEXAHEDRAL MESHING_GEAR	85	24	46	45	52.94%	7.06%	26	30.59%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_CUBESPIKES_MODEL_OUT	111	28	107	101	90.99%	9.35%	34	30.63%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_CUBESPIKES_POLYCUBE_OUT 2015 - DRACTICAL HEY MESU DOTINIZATION VIA EDGE CONCE PECTHECATION BLOCK IN	100	28	107	101	90.99%	9.35%	34	30.63%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION BLOCK_IN 2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION BLOCK_OIT	100	31	100	98	98%	2.08%	31	31%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_BLOCK_STRESSTEST_IN	100	31	100	98	98%	2.08%	31	31%
2015 - PRACTICAL HEX-MESH OPTIMIZATION VIA EDGE-CONE RECTIFICATION_BLOCK_STRESSTEST_OUT	100	31	100	98	98%	2.08%	31	31%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_HAND7_1	67	21	46	40	59.7%	17.8%	21	31.34%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_HAND/_2 2016 - DOUVLUE SUMMUEICAS AND LEO CANSE LAVUETO AS SUBJACES AND VOLUMES BLOCK MODEL OUT	67	19	46	40	59.7%	17.8%	21	31.34%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LATOUTS OF SUFFACES AND VOLUMES BLOCK POLYCUBE OUT	100	33	100	98	98%	2.08%	33	33%
2019 - Symmetric Moving Frames_hex_brokenbullet	24	7	20	17	70.83%	12.37%	8	33.33%
2016 - Structured Volume Decomposition via Generalized Sweeping_kitten_with_bifur_1	26	5	22	22	84.62%	10.53%	9	34.62%
2019 - DUAL SHEET MESHING - AN INTERACTIVE APPROACH TO ROBUST HEXAHEDRALIZATION_ROD	43	16	40	36	83.72%	8.18%	15	34.88%
2016 - EFFCIENT VOLUMETRIC POLYCUBE-MAR CONSTRUCTION_SPHINX_HEX-F 2016 - SEGLETON-DIVEN A DAPTIVE HEX-MEDDA IL MEGNING OF THEIL AD SUADES EEDTH ITY	30	10	23	23	76.67%	11.11%	11	36.67%
2017 - EXPLICIT CYLINDRICAL MAPS FOR GENERAL TUBULAR SHAPES FEMUR	38	12	32	30	78.95%	16.44%	14	36.84%
2016 - Skeleton-driven Adaptive Hexahedral Meshing of Tubular Shapes_santa	42	13	40	38	90.48%	8.24%	16	38.1%
2016 - Skeleton-driven Adaptive Hexahedral Meshing of Tubular Shapes_block	36	14	36	34	94.44%	5.88%	14	38.89%
2016 - POLYCUBE SIMPLIFICATION FOR COARSE LAYOUTS OF SURFACES AND VOLUMES_TABLE2_POLYCUBE_OUT 2016 - STRUCTURE VOLUME DECONFIGURATION UNLED SWEEDING, OUT 2, 2017 2, 2	59	19	58	53	89.83%	8.62%	23	38.98%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_CAT_2	5	2	5	5	100%	0%	2	40%
2016 - Structured Volume Decomposition via Generalized Sweeping_Dolphin_1	5	2	5	5	100%	0%	2	40%
2016 - Structured Volume Decomposition via Generalized Sweeping_Dolphin_2	5	2	5	5	100%	0%	2	40%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_DOLPHIN_3	5	2	5	5	100%	0%	2	40%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_FEMURI_2 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_FEMURI_3	5	2	5	5	100%	0%	2	40%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_FRINKT_5	5	2	5	5	100%	40%	2	40%
2016 - Structured Volume Decomposition via Generalized Sweeping_rabbit_2	5	2	5	5	100%	0%	2	40%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_RABBIT_3	5	2	5	5	100%	0%	2	40%
2017 - EXPLICIT CYLINDRICAL MAPS FOR GENERAL TUBULAR SHAPES_CYLINDER_MIXED 2017 - EXPLICIT CYLINDRICAL MAPS FOR CENERAL TUBULAR SHAPES_CYLINDER_MIXED	7	3	7	7	100%	0%	3	42.86%
2017 - EXPLICIT CTELIDRICAL MAPS FOR GENERAL FOBULAR SHAPES_CTELIDREE_MIAED_W_LORSION 2019 - Diata Sheft Meshing, An Interactive Appendent to Robitst Heyahefbra Lization Robe	16	6	12	12	75%	4 26%	7	42.80%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_BUNNY_1	18	8	16	16	88.89%	6.74%	8	44.44%
2016 - Structured Volume Decomposition via Generalized Sweeping_bunny_2	18	8	16	16	88.89%	6.74%	8	44.44%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_BUNNY6_1	18	8	16	16	88.89%	6.74%	8	44.44%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_BUNNY6_2 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_BUNNY6_2	18	8	16	16	88.89%	6.74%	8	44.44%
2010 - STRUCTORED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_BOUNTO_5 2019 - STRUCTORED VOLUME ASSED HEXAREDRAL MESHING_COLUMN 2019 - SEFECTIVE PADDING FOR POLYCINE-RASSED HEXAREDRAL MESHING_COLUMN	18	8	18	17	94 44%	3.85%	8	44.44%
2016 - All-Hex Meshing Using Closed-Form Induced Polycube_nut-hex	12	6	12	12	100%	0%	6	50%
2019 - Symmetric Moving Frames_hex_tetrahedron	4	2	4	4	100%	0%	2	50%
2017 - EXPLICIT CYLINDRICAL MAPS FOR GENERAL TUBULAR SHAPES_SPRING	7	4	7	7	100%	0%	4	57.14%
2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCUBE_FANCY_RING-HEX 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEDING CAT 1	5	3	5	5	100%	14.29%	3	60%
2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING_CAL_1 2016 - STRUCTURED VOLUME DECOMPOSITION VIA GENERALIZED SWEEPING FEMUR1 1	5	3	5	5	100%	0%	3	60%
2016 - Structured Volume Decomposition via Generalized Sweeping_kitten_1	5	3	5	5	100%	40%	3	60%
2016 - Structured Volume Decomposition via Generalized Sweeping_rabbit_1	5	3	5	5	100%	0%	3	60%
2019 - DUAL SHEET MESHING - AN INTERACTIVE APPROACH TO ROBUST HEXAHEDRALIZATION_DOUBLE-TORUS	5	3	5	5	100%	0%	3	60%
2017 - DAFLICH UTLINDRICAL MAYS FOR GENERAL TUBULAR SHAPES_FEMUR_SHELLU 2016 - ALL-HEX MESHING USING CLOSED-FORM INDUCED POLYCURF KPDLOFKR-HEX	8	2	8	8	100%	38.46%	2	100%
2017 - EXPLICIT CYLINDRICAL MAPS FOR GENERAL TUBULAR SHAPES CYLINDER GRID	1	1	- 1	1	100%	0%	1	100%
2017 - EXPLICIT CYLINDRICAL MAPS FOR GENERAL TUBULAR SHAPES_CYLINDER_POLAR	1	1	1	1	100%	0%	1	100%
2018 - FUZZY CLUSTERING BASED PSEUDO-SWEPT VOLUME DECOMPOSITION FOR HEXAHEDRAL MESHING_EXAMPLE_5	1	1	1	1	100%	0%	1	100%

Table C: Statistics on a dataset of hexahedral meshes. Numbers of blocks in the base complex (BC), reduced base complex (BC⁻), raw motorcycle complex (raw), reduced motorcycle complex with preserved singularity-adjacent walls (MC^+), fully reduced motorcycle complex (MC), percentage of arcs that are T-arcs (T).

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Figure A: Hexahedral meshes of varying density generated by the described quantization method based on the proposed motorcycle complex.

D. Quantization Control

In addition to Fig. 15, Fig. A shows further examples of the ability to control the density of hexahedral meshes resulting from our quantization procedure in a fine-grained manner. To extend the range of test cases beyond those available in the dataset from Table 2 for these examples, we reconstructed seamless parametrizations from given hexahedral meshes: a tetrahedral mesh was generated, containing the singular edges, and a parametrization was imposed on it under which each hex is a unit cube. These seamlessly parametrized tetrahedral meshes can then be taken as input to the quantization procedure like those from the Table 2 dataset.

Fig. B illustrates that when basing the quantization system on the base complex rather than the motorcycle complex, density control may be significantly less fine-grained. This is intimately related to the lower number of degrees of freedom in the conforming structure of the base complex (cf. Fig. 14).



Figure B: Mesh resolution can be controlled more finely when using the MC, not the BC, as basis for quantization using standard objective (10). This is illustrated here for model EXAMPLE_2 (Fig. A bottom center). The number of hexahedra in the extracted hex mesh is shown versus the scaling factor (i.e., target hex edge length is 1/s). The gray line is the conceptual optimum: the number of resulting hexes exactly antiproportional to the target hex volume.